Designing and Testing an Ultrasonic Sensor

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ABSTRACT
A digital ultrasonic sensor will be built and designed by using a piezoelectric transducer, it will be capable of locating nearby objects.

INTRODUCTION & KEY NOTIONS
Ultrasound is defined as a periodic sound pressure with a frequency greater than the upper boundary of the human hearing, typically greater than 20 kHz.

Various current technologies make use of ultrasonic waves, some examples are material testing or medical use. In this report we will be using it to what is known as ultrasound identification (UID).

UID devices conform a part of real time locating systems (RTLS) where the objects in the neighborhood are used to bounce back the signal and then with some calculations obtain information of their position (Fig. 1).

DESIGN
The required stages for our sensor will be summarized by block diagram. (Fig. 2).

The emitter and receiver will operate at a frequency of approximately 40 KHz. The components to be used are labeled as TC-T40-16 and after some measurements we can see they have an impedance of around 1.2 Ω.

There are two main analog blocks in this system;

a) The filter – which will be a low-pass 50 kHz filter to prevent aliasing in the analog-to-digital conversion.

b) Amplifier – that needs to amplify and give enough power to the piezoelectric sender.

Because ultrasound signals have short wavelengths the sensors are confined for more precise locations.
The low-pass filter will be implemented with a 4th Order Sallen-Key topology by cascading two 2nd Order stages (Fig. 3).

![2nd Order Sallen-Key](image)

Fig. 3: 2nd Order Sallen-Key.

And finally, the amplifier stage will include a non-inverting amplifier coupled with a Class B stage in crossover-distortion correction feedback configuration (Fig. 5).

![Non-inverting amplifier with power output](image)

Fig. 4: Non-inverting amplifier with power output.

The filter to implement will be Butterworth, so according to the normalized tables:

<table>
<thead>
<tr>
<th>Stage</th>
<th>$a_1$</th>
<th>$b_i$</th>
<th>$Q_i$</th>
</tr>
</thead>
<tbody>
<tr>
<td>1st</td>
<td>1.8478</td>
<td>1.0000</td>
<td>0.54</td>
</tr>
<tr>
<td>2nd</td>
<td>0.7654</td>
<td>1.0000</td>
<td>1.3100</td>
</tr>
</tbody>
</table>

Where in relationship to the previous table, the transfer function is shown in equation (1).

$$H(s) = \frac{1}{b_1 s^2 + a_1 s + 1}$$

where for a Sallen-Key configuration with unity gain;

$$b_i = C_1 C_2 R_2 R_3 \quad , \quad \omega_o = \frac{1}{\sqrt{b_i}} = \frac{1}{\sqrt{C_1 C_2 R_2 R_3}} \quad \text{or}$$

$$f_o = \frac{1}{2 \pi \sqrt{R_1 R_2 C_1 C_2}} \quad \text{and} \quad Q = \frac{\sqrt{R_1 R_2 C_1 C_2}}{(R_1 + R_2) C_2}$$

We start by calculating the values for the first stage:

$$C_1 = 1 \quad , \quad C_2 = n \quad , \quad R_1 = R \quad , \quad R_2 = mR$$

then $$\omega_o = 1$$ and $$m = \frac{1}{2 \pi \omega_o Q} - 1$$.

If we define $$R = 0.1$$ then $$m = 1.947$$ and $$n = \frac{1}{m} \left( \frac{1}{2 \pi R \omega_o} \right)^2 = 1.30$$.

And finally for the second and final stage:

$$C_1 = 1 \quad , \quad C_2 = n \quad , \quad R_1 = R \quad , \quad R_2 = mR$$

then $$\omega_o = 1$$ and $$m = \frac{1}{2 \pi \omega_o Q} - 1$$.

If we define $$R = 0.01$$ then $$m = 11.149$$ and $$n = \frac{1}{m} \left( \frac{1}{2 \pi R \omega_o} \right)^2 = 22.72$$.
The normalized values to 1 Hz then can be summarized in the following tables.

<table>
<thead>
<tr>
<th>1st Stage</th>
<th></th>
</tr>
</thead>
<tbody>
<tr>
<td><strong>R_1</strong></td>
<td>0.1 Ω</td>
</tr>
<tr>
<td><strong>R_2</strong></td>
<td>0.1947 Ω</td>
</tr>
<tr>
<td><strong>C_1</strong></td>
<td>1 F</td>
</tr>
<tr>
<td><strong>C_2</strong></td>
<td>1.3 F</td>
</tr>
</tbody>
</table>

<table>
<thead>
<tr>
<th>2nd Stage</th>
<th></th>
</tr>
</thead>
<tbody>
<tr>
<td><strong>R_1</strong></td>
<td>0.01 Ω</td>
</tr>
<tr>
<td><strong>R_2</strong></td>
<td>0.01 Ω</td>
</tr>
<tr>
<td><strong>C_1</strong></td>
<td>1 F</td>
</tr>
<tr>
<td><strong>C_2</strong></td>
<td>22.72 F</td>
</tr>
</tbody>
</table>

Normalizing to commercial values (Fig. 5) with software we obtain:

![Fig. 5: 4th Order Butterworth low-pass filter @ 50 kHz.](image)

With a frequency response in the next figures (Fig. 6 & Fig. 7).

Fig. 6: Low-pass frequency response.

Since the system will be fed a square signal of 3.3 Volts in amplitude with the first fundamental frequency of 40 kHz, then the amplifying stage will have an approximate gain of \(3 \text{V/V} \), therefore the following circuit will be implemented (Fig. 7).

![Fig. 7: Zoom-in the frequency response.](image)

Fig. 7: Zoom-in the frequency response.

With the amplified pulse on our emitter we are able to increase the range of the sensor.

![Fig. 8: Amplifier and power stage.](image)

Fig. 8: Amplifier and power stage.
CONCLUSIONS

Analog systems and implementations are greatly required on every-day devices. The mixing of analog and digital systems offer a great combination in the field of applied electronics. One thing to take note is that moderately cheap and really innovative appliances can be built with well thought and designed systems.

Ultrasound detection can be greatly improved with well thought processing algorithms that make up for defects in the simplest method, while analog maintain special properties such as continuous-time speed (in a sense) and some implementations may be cheaper which helps reduce the overall system cost.

REFERENCES


